## Homework 1 Solutions

Here we have the homework \#1 solutions, preceeded by a few imports from the (almost) standard library and the definition of an utility function.

In [1]: import numpy as np from numpy import cos, exp, pi, sin, sqrt
def $p d(s, v, u=$ None $)$ :
if $u$ :
print('\%30s: \%g [\%s]'\%(s, v, u))
else:
print('\%30s: \%g'\%(s, v))

## System Identification

The data, first as in text, next a bit of manipulation to have different values in different arrays

In [2]:

```
# f P P rho theta
raw = [[18., 3240., 54., 24.3],
    [20., 4000., 118., 55.1],
    [22., 4840., 132., 123.9],
    [24., 5760., 80., 152.5]]
f, p, r, t = map(np.array, zip(*raw))
omega = f*2*pi
force = p
rho = r/1E6
theta = t*pi/180.0
```

$A$ is the matrix of coefficients and $b$ the known term, $k$ and $m$ are computed using a least squares solver

In [3]: $A=n p . v s t a c k((n p . o n e s(4)$, -omega**2)).T
b = force*cos(theta)/rho
$\mathrm{k}, \mathrm{m}=\mathrm{np}$.linalg.lstsq(A, b, rcond=None) [0]

In [4]: print('Matrix of coefficients, \n[ 1, -omega^2_i ]')
print('\n'.join('[ \%d, \%.4g ]'\%(row[0], row[1]) for row in A))
print('Known term, p_i•cos theta_i/rho_i,')
print('[', ', '.join('\%.4g'\%x for $x$ in b), ']\n')
print('Stiffness [MN/m]', k/1E6)
print(' Mass [ton]', m/1000)
Matrix of coefficients,
[ 1, -omega^2_i ]
$[1,-1.279 \mathrm{e}+04]$
[ 1, $-1.579 \mathrm{e}+04$ ]
$[1,-1.911 \mathrm{e}+04]$
[ 1, -2.274e+04 ]
Known term, p_i.cos theta_i/rho_i,
[ $5.468 \mathrm{e}+07,1.939 \mathrm{e}+07,-2.045 \mathrm{e}+\overline{0} 7,-6.386 \mathrm{e}+07$ ]
Stiffness [MN/m] 207.45835123684353
Mass [ton] 11.927812957251826

First we print the four estimates of $\zeta$ from the four imprecise measurements, next the estimate obtained using the least squares solver.

In [5]:

```
wn2 = k/m
wn = sqrt(wn2)
beta = omega/wn
])
[ 0.06939, 0.07032, 0.06998, 0.07008 ]
```

print('[', ', '.join('\%.4g'\%x for $x$ in (force*sin(theta)/(2*rho*k*beta))), ']')
print(np.linalg.lstsq(np.ones( $(4,1))$, force*sin(theta)/(2*rho*k*beta), rcond=None)[0][0
0.06994247277376539
Let's say that $\zeta=7 \%$.

## Vibration Isolation

The data, some easily derived quantity. beta 2 is the squared frequency ratio of the undamped, isolated system.

In [6]: mass $=17.13 \mathrm{E} 3$
freq $=10.0$
omega $=$ freq*2*pi
$T R=1 / 3$
beta2 $=1+1 /$ TR

The frequency ratios ofthe damped systems are found using a library root solver, a bit of cheating isn't it?

Next, the stiffnesses for different dampings are $k=m \omega_{n}^{2}=m \omega^{2} / \beta^{2}$.

In [7]: from scipy.optimize import newton

```
def tr(b, z): return sqrt(1+4*b*b*z*z)/sqrt((1-b*b)**2+4*z*z*b*b)
b_01 = newton(lambda b: tr(b, 0.01)-TR, sqrt(beta2))
b_10 = newton(lambda b: tr(b, 0.10)-TR, sqrt(beta2))
k_00 = mass*omega**2/beta2
k_01 = mass*omega**2/b_01**2
k_10 = mass*omega**2/b_10**2
```

In [8]: print("Damping Ratio, Damping Coeff. [kN•s/m], Stiffness [MN/m]")

$$
\text { print(" } \quad 0 \% \%, \% 25.3 f, \% 19.3 f " \%(0.0, \text { k_00/1E6)) }
$$

print(" 1\%\%, \%25.3f, \%19.3f"\%(
0.02*sqrt(k_01*mass)/1000, k_01/1E6))
print(" $10 \% \%$, \%25.3f, \%19.3f"\%(
0.20*sqrt(k_10*mass)/1000, k_10/1E6))

Damping Ratio, Damping Coeff. [kN•s/m], Stiffness [MN/m]

| $0 \%$, | 0.000, | 16.907 |
| ---: | ---: | ---: |
| $1 \%$, | 10.760, | 16.898 |
| $10 \%$, | 104.824, | 16.036 |

## Impulsive Load + Num.Integration

The data of the problem and some easily derived parameters

```
In [9]: mass = 400
wn = 2*pi*4
z = 0.03
p0 = 8200.0
t0 = 0.040
stif = mass*wn**2
damp = 2*z*wn*mass
Tn = 2*pi/wn
beta = Tn/2/t0
Dst = p0/stif
```

We have a formula for the maximum of free response for a half sine excitation...

In [10]: Rmax $=2 *$ beta*cos(pi/2/beta)/(beta**2-1)
xmax_00_exact $=$ Dst*Rmax
print('Exact formula for undamped system')
pd('Static displacement', Dst*1000, 'mm')
pd('Max response coeff.', Rmax)
pd('Max displacement', xmax_00_exact*1000, 'mm')
Exact formula for undamped system
Static displacement: 32.4544 [mm]
Max response coeff.: 0.624818
Max displacement: 20.2781 [mm]

Now the approximate formula, valid for every type of short impulse. The integral of the half sine is

$$
p_{0} \int_{0}^{t_{0}} \sin \left(\pi \tau / t_{0}\right) d \tau=2 p_{0} t_{0} / \pi
$$

In [11]: print('Impulse-momentum approximate result') integral $=$ p0*2*t0/pi
xmax_00_approx = integral/mass/wn
pd('Max displacement', xmax_00_approx*1000, 'mm')
Impulse-momentum approximate result
Max displacement: 20.7708 [mm]

And the numerical solution (now we take into account the damping).
We choose a total duration, a time step, we instantiate a time vector and define the loading and the load increments.

In [12]: $\mathrm{t} 1=0.100$
$N=1000$
$h=t 1 / N$
$\mathrm{t}=\mathrm{np}$.linspace $(0, \mathrm{t} 1, \mathrm{~N}+1$ )
$\mathrm{p}=\mathrm{p} 0^{*} \mathrm{np}$. where $(\mathrm{t}<=\mathrm{t} 0, \sin (\mathrm{pi} * \mathrm{t} / \mathrm{t} 0), 0.0)$
$\mathrm{Dp}=\mathrm{p}[1:]-\mathrm{p}[:-1]$

The constants for the Constant Acceleration Algorithm (they depend on $h$ )

In [13]

```
ks = stif + 2*damp/h + 4*mass/h/h
cs = 2*damp + 4*mass/h
ms = 2*mass
```

so that in the next slide we can compute the solution (up to the point of a velocity reversal).

In [14]:

```
x0, v0 = 0, 0
for tt, p0, dp in zip(t, p, Dp):
    a0 = (p0-damp*v0-stif*x0)/mass
    dps = dp+ms*a0+cs*v0
    dx = dps/ks
    dv = 2*(dx/h-v0)
    x0, v0 = x0+dx, v0+dv
    if v0<0: break
pd('Max displacement', x0*1000, 'mm')
```

Max displacement: 19.3616 [mm]

## Rayleigh Quotient and Refinements

The data of the problem, in order the assumed displacements, the floor masses and the storey stiffnesses. We define also a fictitious frequency and its square and eventually we import the Fraction class from the standard library for a later use.

In [15]:

```
x0, x1, x2, x3 = 0, 1, 2, 3
m1, m2, m3 = 5, 5, 3
k1, k2, k3 = 8, 5, 2
w = 1 ; w2 = w*w
from fractions import Fraction as f
```

To compute the (double of the) strain energy we need the storey deflections, d1 etc.
The $R Q$ is simply the fraction ( $f$, that is) with $V 2$ in the numerator and $T 2$ in the denominator.

```
In [16]: d1, d2, d3 = x1-x0, x2-x1, x3-x2
V2 = k1*d1**2 + k2*d2**2 + k3*d3**2
T2 = w**2 * (m1*x1**2 + m2*x2**2 + m3*x3**2)
R00 = f(V2,T2)
```

To proceed with refinements we need the inertial forces ( f 1 , etc), the storey shears (v1, etc, note that we have to sum the floor forces from the top to the bottom), the storey deflections (d1, etc, computed as exact fractions using f) and eventually the floor displacements ( x 1 , etc, this time we sum from the bottom to the top).

In [17]:

```
f1, f2, f3 = w2*m1*x1, w2*m2*x2, w2*m3*x3
print("Inertial forces, f_i/(m w**2)", f1, f2, f3)
v3 = f3 ; v2 = v3+f2 ; v1 = v2+f1
print("Storey shears, F_i/(m*w**2) ", v1, v2, v3)
d1, d2, d3 = f(v1, k1), f(v2, k2), f(v3, k3)
print("Storey deflections, d_i*k/(m*w**2)", d1, d2, d3)
x1 = x0+d1 ; x2 = x1+d2 ; x3 = x2+d3
print("Storey displacements, x_i*k/(m*w**2)", x1, x2, x3)
```

Inertial forces, f_i/(m w**2) 5109
Storey shears, F_i/(m*w*2) 24199
Storey deflections, d_i*k/(m*w*2) 3 19/5 9/2
Storey displacements, x_i*k/(m****2) 3 34/5 113/10

With the new displacements and the old forces, estimate a better V2 and next compute R01 and eventually a better kinetic energy T2 and R11.

In [18]:

```
V2 = f1*x1 + f2*x2 + f3*x3
R01 = f(T2, V2)
T2 = w2*( m1*x1**2 + m2*x2**2 + m3*x3**2)
R11 = f(V2, T2)
```

It's time to display our results

In [19]: def p_Rxx(Rs, Rv):
print('\%10s $\left.=\% 15 \mathrm{~s} k / \mathrm{m}=\% \mathrm{k} / \mathrm{m} .{ }^{\prime} \%(\mathrm{Rs}, \operatorname{str}(\mathrm{Rv}), 1.0 * R v)\right)$
p_Rxx('R00', R00)
p_Rxx('R01', R01)
p_Rxx('R11', R11)
$\begin{array}{lrl}\text { R00 }= & 15 / 52 \mathrm{k} / \mathrm{m}=0.288462 \mathrm{k} / \mathrm{m} . \\ \text { R01 }= & 520 / 1847 \mathrm{k} / \mathrm{m}=0.281538 \mathrm{k} / \mathrm{m} . \\ \text { R11 }= & 18470 / 65927 \mathrm{k} / \mathrm{m}=0.280158 \mathrm{k} / \mathrm{m} .\end{array}$

